

# NASA TN D-6026

c./

LOAN COPY: RETURN AFWL (WLOL) N

CH LIBRARY KAFB, NM

OL32783

# GROWTH DUE TO BUOYANCY OF WEAK HOMOGENEOUS TURBULENCE WITH SHEAR

by Robert G. Deissler Lewis Research Center Cleveland, Ohio 44135

NATIONAL AERONAUTICS AND SPACE ADMINISTRATION . WASHINGTON, D. C. . OCTOBER 1970

TECH LIBRARY KAFB, NM

1 [



				בסופרת
1. Report No. NASA TN D-6026	2. Government Access	sion No.	3. Recipient's Catalog	No.
4. Title and Subtitle			f Bood Date	
			5. Report Date October 1970	
GROWTH DUE TO BUOYANC	Y OF WEAK HOM	OGENEOUS	6. Performing Organiz	
TURBULENCE WITH SHEAR			-	
7. Author(s)			8. Performing Organiza	ation Report No.
Robert G. Deissler			E-5676	
			10. Work Unit No.	-
Performing Organization Name and Address			129-01	
Lewis Research Center	Ţ	11. Contract or Grant	No.	
National Aeronautics and Space	ce Administration			}
Cleveland, Ohio 44135			13. Type of Report an	d Period Covered
12. Sponsoring Agency Name and Address			Technical No	te
National Aeronautics and Space Administration		Ţ.	14. Sponsoring Agency	Code
Washington, D.C. 20546				
15. Supplementary Notes	-	<del>-</del>		
16. Abstract				
An analysis is made to determ				
and shear changes with time.	It is shown that,	although the turbule	nce ultimately d	ecays when
buoyancy is absent, the prese	nce of buoyancy co	ounteracts the decay	, and the turbule	ent energy
grows at large times.				
				į
17. Key Words (Suggested by Author(s))		18. Distribution Statement		
	near	Unclassified - unlimited		
Homogeneous G:	rowth			
Buoyancy				
19. Security Classif. (of this report)	20. Security Classif. (	of this page)	21. No. of Pages	22. Price*

# GROWTH DUE TO BUOYANCY OF WEAK HOMOGENEOUS TURBULENCE WITH SHEAR by Robert G. Deissler Lewis Research Center

# **SUMMARY**

An analysis is made to determine how the energy in a weak homogeneous turbulence with buoyancy and shear changes with time. It is shown that, although the turbulence ultimately decays when buoyancy is absent, the presence of buoyancy counteracts the decay, and the turbulent energy grows at large times.

# INTRODUCTION

Studies of weak homogeneous (grid generated) turbulence with uniform mean velocity gradient are given in references 1 and 2. In the results obtained there, the turbulent energy always decayed with time. The energy produced by the mean velocity gradient was at all times less than that dissipated. In reference 3, where the initial condition was modified to give a finite initial turbulent energy, the energy sometimes increased for a while, but it still ultimately decayed. This behavior was attributed to the fact that, while the total energy was increasing, energy was being drained out of the component of the turbulence in the direction of the velocity gradient by the pressure-velocity correlations. Since there was no turbulence production in that component, it quickly decayed, with the result that the turbulent shear stress, and consequently the turbulence production in all the components, ultimately decreased.

Thus, the key to obtaining a nondecaying turbulent shear flow appears to lie in keeping the energy from being drained out of the turbulence component in the direction of the mean velocity gradient. In strong turbulence, the distribution of energy among the directional components is evidently accomplished by the pressure-velocity correlations, but in weak turbulence, those correlations generally tend to make the turbulence more anisotropic (ref. 1). If, however, we superimpose on the shear flow destabilizing buoyancy forces in the direction of the mean velocity gradient, it may be possible to

obtain a nondecaying solution, even for weak turbulence. Those buoyancy forces should tend to prevent the turbulence component in the direction of the mean velocity gradient from decaying.

Some of the effects of combined buoyancy and shear on weak homogeneous turbulence were investigated in reference 4. However, the question of whether or not the turbulence decays was not considered. It is with that aspect of the problem that we will be concerned here.

## ANALYSIS

The basic equations for the present study can be written as (ref. 4)

$$\frac{\partial \mathbf{u_i}}{\partial t} + \mathbf{u_k} \frac{\partial \mathbf{U_i}}{\partial \mathbf{x_k}} + \mathbf{U_k} \frac{\partial \mathbf{u_i}}{\partial \mathbf{x_k}} + \frac{\partial (\mathbf{u_i u_k})}{\partial \mathbf{x_k}} - \frac{\partial \overline{\mathbf{u_i u_k}}}{\partial \mathbf{x_k}} = -\frac{1}{\rho} \frac{\partial (\mathbf{p - p_e})}{\partial \mathbf{x_i}} + \nu \frac{\partial^2 \mathbf{u_i}}{\partial \mathbf{x_k} \partial \mathbf{x_k}} - \beta \mathbf{g_i \tau}$$
(1)

$$\frac{1}{\rho} \frac{\partial^{2}(p - p_{e})}{\partial x_{i} \partial x_{i}} = -2 \frac{\partial u_{i}}{\partial x_{k}} \frac{\partial U_{k}}{\partial x_{i}} - \frac{\partial^{2}(u_{i}u_{k})}{\partial x_{i} \partial x_{k}} + \frac{\partial^{2}\overline{u_{i}u_{k}}}{\partial x_{i} \partial x_{k}} - \beta g_{i} \frac{\partial \tau}{\partial x_{i}}$$
(2)

and

$$\frac{\partial \tau}{\partial t} + u_k \frac{\partial T}{\partial x_k} + U_k \frac{\partial \tau}{\partial x_k} + \frac{\partial (\tau u_k)}{\partial x_k} - \frac{\partial \overline{\tau u_k}}{\partial x_k} = \alpha \frac{\partial^2 \tau}{\partial x_k \partial x_k}$$
(3)

where the subscripts (except e) can take on the values 1, 2, or 3, and a repeated subscript in a term signifies a summation. The quantity  $\mathbf{u_i}$  is a fluctuating velocity component,  $\mathbf{t}$  is the time,  $\mathbf{U_i}$  is a mean velocity component,  $\rho$  is the density,  $\mathbf{p}$  is the instantaneous pressure,  $\mathbf{p_e}$  is the equilibrium pressure,  $\mathbf{x_i}$  is a space coordinate,  $\nu$  is the kinematic viscosity,  $\beta = -(1/\rho)(\partial \rho/\partial T)_p$ ,  $\mathbf{g_i}$  is a component of the body force per unit mass,  $\tau$  is the temperature fluctuation,  $\mathbf{T}$  is the mean temperature,  $\alpha$  is the thermal diffusivity, and overbars designate averaged values. (Symbols are defined in the appendix.)

In obtaining equations (1) to (3), the instantaneous velocities and temperatures in the incompressible Navier-Stokes and energy equations are broken into mean and fluctuating components. For the last term in equation (1) (buoyancy term), the density is assumed to depend effectively only on temperature and is not far removed from its equilibrium value (value it would have for no heat transfer or turbulence). The equation for the pressure (eq. (2)) is obtained by taking the divergence of the Navier-Stokes equation and applying continuity.

Equations involving correlations between fluctuating quantities at two points P and P' can be constructed from equations (1) to (3). Such equations have been obtained for homogeneous turbulence with uniform velocity and temperature gradients in reference 4. They can be converted to spectral form by taking their Fourier transforms. We consider the case where the velocity and temperature gradients are in the  $x_3$ -direction (vertical) and the body force (gravity) is in the  $-x_3$ -direction. Let  $g = -g_3$ ,  $a = dU_1/dx_3$ , and  $b = dT/dx_3$ , and assume that the turbulence is weak enough to neglect terms containing triple correlations. The correlation equations then become in spectral form

$$\frac{\partial \varphi_{ij}}{\partial t} - a\kappa_{1} \frac{\partial \varphi_{ij}}{\partial \kappa_{3}} = -a(\delta_{i1}\varphi_{j3} + \delta_{1j}\varphi_{i3}) + 2a\left(\frac{\kappa_{1}\kappa_{j}}{\kappa^{2}}\varphi_{i3} + \frac{\kappa_{i}\kappa_{1}}{\kappa^{2}}\varphi_{j3}\right) + \beta g\gamma_{i}\left(\delta_{j3} - \frac{\kappa_{3}\kappa_{j}}{\kappa^{2}}\right) + \beta g\gamma_{j}\left(\delta_{i3} - \frac{\kappa_{i}\kappa_{3}}{\kappa^{2}}\right) - 2\nu\kappa^{2}\varphi_{ij}$$

$$+ \beta g\gamma_{j}\left(\delta_{i3} - \frac{\kappa_{i}\kappa_{3}}{\kappa^{2}}\right) - 2\nu\kappa^{2}\varphi_{ij}$$

$$(4)$$

$$\frac{\partial \gamma_{i}}{\partial t} - a\kappa_{1} \frac{\partial \gamma_{i}}{\partial \kappa_{3}} = -b\varphi_{i3} + a\gamma_{3} \left(2 \frac{\kappa_{i}\kappa_{1}}{\kappa^{2}} - \delta_{i1}\right) + \beta g\delta \left(\delta_{i3} - \frac{\kappa_{i}\kappa_{3}}{\kappa^{2}}\right) - (\alpha + \nu)\kappa^{2}\gamma_{i}$$
 (5)

$$\frac{\partial \delta}{\partial t} - a\kappa_1 \frac{\partial \delta}{\partial \kappa_3} = -2b\gamma_3 - 2\alpha\kappa^2\delta \tag{6}$$

where  $\varphi_{ij}$ ,  $\gamma_i$ , and  $\delta$  are given by

1

Ĩ,

1

$$\overline{\mathbf{u}_{i}\mathbf{u}_{j}'} = \int_{-\infty}^{\infty} \varphi_{ij} e^{i\vec{\kappa} \cdot \vec{\mathbf{r}}} d\vec{\kappa}$$
(7)

$$\overline{\tau u_{i}'} = \int_{-\infty}^{\infty} \gamma_{i} e^{i\vec{\kappa} \cdot \vec{r}} d\vec{\kappa}$$
 (8)

$$\overline{\tau \tau'} = \int_{-\infty}^{\infty} \delta e^{i\vec{\kappa} \cdot \vec{r}} d\vec{\kappa}$$
 (9)

The quantity  $\vec{\kappa}$  is the wave number vector and  $d\vec{\kappa} = d\kappa_1 d\kappa_2 d\kappa_3$ . The magnitude of  $\vec{\kappa}$  has the dimension 1/length and can be considered to be the reciprocal of a wavelength or eddy size. The unprimed and primed quantities in the barred products refer, respectively, to values at points P and P' separated by the vector r. The quantity  $\delta_{ij}$  is the Kronecker delta.

Equations (4), (5), and (6) give contributions of various processes to the rate of change of spectral components of  $\overline{u_i u_j}$ ,  $\overline{\tau u_i}$ , and  $\overline{\tau^2}$ , respectively. The second term in each equation is a transfer term which transfers activity into or out of a spectral component by the stretching or compressing of turbulent vortex filaments by the mean velocity gradient, as discussed in reference 1. The terms with  $\kappa^2$  in the denominator are spectral components of pressure-velocity or pressure-temperature correlations and transfer activity between directional components (ref. 1). The terms proportional to  $\beta g$  and  $\delta_{i3}$  (or  $\delta_{j3}$ ) are buoyancy terms which augment or diminish the activity in a spectral component by buoyant action. The last terms in the equations are dissipation terms, which dissipate activity by viscous or by conduction effects. The remaining terms in the equations produce activity by velocity or temperature gradient effects.

For solving equations (4) to (6), the turbulence is assumed to be initially isotropic at  $t = t_0$ . That condition is satisfied by

$$\varphi_{ij} = \frac{J_0}{12\pi^2} \left( \kappa^2 \delta_{ij} - \kappa_i \kappa_j \right) e^{-\left(\kappa/\kappa_0\right)^2}$$
(10)

where  $J_0$  is a constant that depends on initial conditions and  $\kappa_0$  is an initial wave number that is characteristic of the turbulence. Equation (10) differs from the initial condition in references 1, 2, and 4 (but not from that in 3) by the exponential factor, which was set equal to 1 in those references ( $\kappa_0 = \infty$ ). For the initial conditions on  $\delta$  and  $\gamma_i$  (at  $t = t_0$ ), it is assumed that

$$\delta_0 = \left(\gamma_i\right)_0 = 0 \tag{11}$$

1

ſ

That is, the turbulence producer (grid) is assumed to be unheated, so that the temperature fluctuations are produced by the interactions of the mean temperature gradient with the turbulence.

A method of solving the preceding set of partial differential equations (eqs. (4) to (6)) is described in reference 4. Those equations are converted to ordinary differential equations, and spherical coordinates are introduced by using the transformations

 $\kappa_1 = \kappa \cos \varphi \sin \theta$ ,  $\kappa_2 = \kappa \sin \varphi \sin \theta$ , and  $\kappa_3 = \kappa \cos \theta$ . The resulting set of equations is integrated numerically by machine computation. Directionally integrated spectrum functions can then be obtained from

$$\begin{bmatrix} \psi_{ij} \\ \Gamma_i \\ \Delta \end{bmatrix} = \int_0^{\pi} \int_0^{2\pi} \begin{bmatrix} \varphi_{ij} \\ \gamma_i \\ \delta \end{bmatrix} \kappa^2 \sin \theta \, d\varphi \, d\theta \tag{12}$$

These spectrum functions can be integrated over all wave numbers to give the following single-point correlations:

$$\begin{bmatrix} \overline{u_i u_j} \\ \overline{\tau u_i} \\ \overline{\tau^2} \end{bmatrix} = \int_0^{\infty} \begin{bmatrix} \psi_{ij} \\ \Gamma_i \\ \Delta \end{bmatrix} d\kappa \tag{13}$$

Computed correlations and spectra for the case where the buoyancy forces are destabilizing (negative vertical temperature gradients) will be considered in the next section. The results given there are for a gas with a Prandtl number of 0.7.

## RESULTS AND DISCUSSION

The effect of destabilizing buoyancy forces on weak homogeneous shear-flow turbulence in a gas is illustrated in figure 1. The superscript (a) on  $\overline{u_i u_j}(a)$ ,  $t^{(a)}$ , and  $\kappa_0^{(a)}$  indicates that those parameters have been made dimensionless by using quantities related to the shear (in contrast to those related to the buoyancy, which will be used later). Curves are shown for two values of Richardson number and of the initial wave number parameter.

The curves indicate that for a Richardson number of 0 (no buoyancy effects) all components of the turbulent energy decrease with time. The turbulent shear stress  $\overline{-u_1u_3}$  also decreases with time, except near the initial time. (At  $t^{(a)}=0$  the turbulence is isotropic and  $\overline{u_1u_3}$  is 0.)

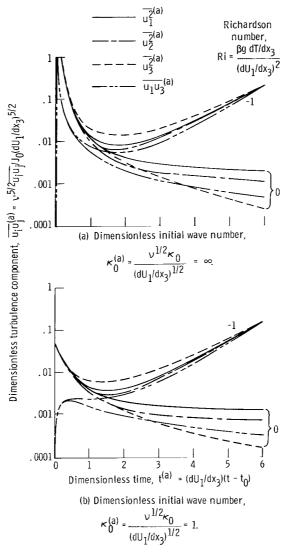


Figure 1. - Effect of destabilizing buoyancy on variation with time of weak turbulence in uniform uniform shear flow. Prandtl number, 0.7.

The decay of the components of turbulent energy for no buoyancy effects evidently occurs mainly because there is no production term in the equation for  $\overline{u_3u_3}$  (component in the direction of the mean velocity gradient). This can be seen by letting i=j=3 in equation (4), in which case the production term (first term on the right side) drops out. In addition, the pressure-velocity correlation terms in equation (4) tend to drain energy out of the  $\overline{u_3^2}$ -component when the turbulence is weak, as discussed in reference 1. As a result the  $\overline{u_3^2}$ -component decays rapidly compared with the other components, which have energy fed into them by the mean velocity gradient or by the pressure-velocity correlations (see fig. 1). When  $\overline{u_3^2}$  decays, the shear component  $\overline{u_3u_1}$  must also de-

cay. There is then no mechanism for maintaining the turbulence since that maintenance apparently takes place as a result of work done on the turbulent shear stress by the velocity gradient. (See first term on right side of eq. (4).) All of the turbulence components must then decay.

By contrast, for Ri = -1 (buoyancy forces destabilizing), all components of the turbulent energy decay for a while and then begin to increase without limit as time becomes large. This increase evidently occurs because the vertical buoyancy forces excite the  $u_3^2$ -component of the turbulence and replenish the energy being drained out of it.

It might seem surprising that all components of the turbulence continue to increase with time rather than level off. There are no boundaries on the flow considered here however, so that the effective Reynolds number and Rayleigh number of the mean flow are infinite. As the scale or mixing length of the turbulence continues to grow, the eddies encounter larger and larger velocity and temperature differences, so that the effective driving forces on the turbulence continue to grow.

Comparison of figures 1(a) and (b) shows, as expected, that for  $\kappa_0^{(a)} = \infty$  (all wave numbers present), the components of the initial energy are infinite, whereas for  $\kappa_0^{(a)} = 1$  they have a finite value. The turbulent shear stress  $-\overline{u_3u_1}$  starts at zero on both plots since the turbulent shear stress for isotropic turbulence is zero. For the case of  $\kappa_0^{(a)} = \infty$ , however, the value of  $-\overline{u_3u_1}$  jumps to infinity in an infinitely short time and then decreases. For  $\kappa_0^{(a)} = 1$ ,  $(-\overline{u_3u_1})$  first increases steadily and then either decreases (Ri = 0) or continues to increase (Ri = -1).

To give an idea of the distribution of the turbulent energy with wave number, energy spectra (spectra of  $\overline{u_i u_i}$ ) are plotted in figure 2 for  $\kappa_0^{(a)} = \infty$  and  $\mathrm{Ri} = 0$  and -1. For  $\mathrm{t}^{(a)} = 0$ ,  $\psi_{ii}$  is proportional to  $\kappa^4$  (eq. (10)). As time increases, the spectra move to the smaller wave number regions; that is, the scale of the turbulence grows indefinitely large with time, since the fluid is unbounded.

Thus far we have been considering the effect of buoyancy on a shear-flow turbulence. Next we want to consider the related problem of the effect of imposing a mean shear on turbulence that is buoyancy-controlled. For doing this it is convenient to use the parameters  $\overline{u_1^2(b)}$ ,  $t^{(b)}$ ,  $\kappa_0^{(b)}$ ,  $\overline{\tau^2(b)}$ , and  $\overline{\tau u_3}^{(b)}$ , which have been made dimensionless by using quantities related to the buoyancy (see figs. 3 and 4). The parameters used in figure 1 were, on the other hand, nondimensionalized by using quantities related to the shear.

The effects of shear on buoyancy-controlled turbulence are illustrated in figure 3 and 4, where  $u_1^2(b)$ ,  $\tau^2(b)$ , and  $\tau u_3(b)$  are plotted against  $t^{(b)}$  for several values of Richardson number and  $\kappa_0^{(b)}$ . For the case of no shear (Ri = - $\infty$ ) the results were obtained from the integrated equations in reference 5. All components of the turbulent energy, as well as the temperature fluctuations and the temperature-velocity correlations, increase as  $t^{(b)}$  becomes large. This occurs even when shear is absent and the

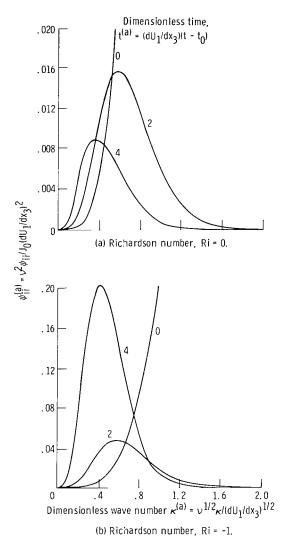


Figure 2. - Variation with time of turbulent energy spectra (spectra of  $\overline{u_i u_i}$ ). Prandtl number, 0.7.

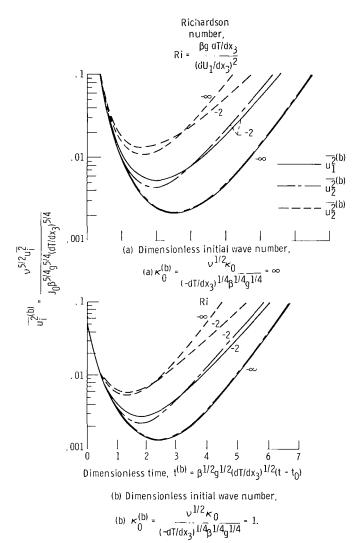
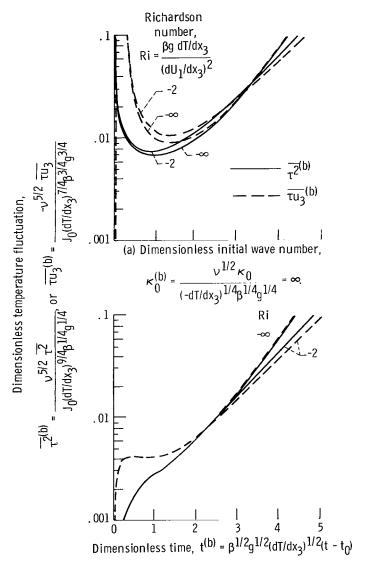


Figure 3. - Effect of uniform shear on variation with time of weak turbulence in flow with destabilizing buoyancy. Prandtl number, 0.7.



(b) Dimensionless initial wave number,

(b) 
$$\kappa_0^{(b)} = \frac{v^{1/2} \kappa_0}{(-dT/dx_3)^{1/4} \beta^{1/4} g^{1/4}} = 1$$

Figure 4. - Effect of uniform shear on variation with time of temperature fluctuations and temperature-velocity correlations in flow with destabilizing buoyancy. Prandtl number, 0.7.

turbulence is completely controlled by the destabilizing buoyancy forces ( $Ri = -\infty$ ). Although all turbulent energy components can increase with time when shear is absent, the component in the direction of the buoyancy forces is, in that case, at least an order of magnitude greater than the other components. On the other hand, when both buoyancy and shear are present, all components can be of the same order of magnitude.

Loeffler has recently considered the effect of a gradient in electric charge and an applied electric field on homogeneous turbulence (ref. 6). That problem is analogous to the present one for the case when no shear is present and the Prandtl number is infinite. It was found that the turbulent energy increases without limit as time increases, when the electric field is in the direction of increasing charge density. For large times the turbulent energy was proportional to  $(\exp t^{(b)})/(t^{(b)})^3$ .

As the shear increases (as Ri goes from  $-\infty$  to -2), the turbulent activity in general increases, at least at the earlier times. The shear does not seem to affect  $\overline{\tau^2}^{(b)}$  or  $\overline{\tau u_3}^{(b)}$  at the smaller times when  $\kappa_0^{(b)} = 1$ , however. At larger times, although  $\overline{u_1^2}$  and  $\overline{u_2^2}$  increase with increasing shear,  $\overline{u_3^2}$ ,  $\overline{\tau^2}$ , and  $\overline{\tau u_3}$  all decrease with increasing shear. These decreases appear to be related to the fact that at large times the presence of the shear causes energy to be drained out of the  $\overline{u_3^2}$  component (as discussed earlier), and thus out of  $\overline{\tau u_3}$  and  $\overline{\tau^2}$  (see eqs. (5) and (6)).

# CONCLUDING REMARKS

Although weak homogeneous turbulence with a uniform shear ultimately decays with time, the presence of destabilizing buoyancy forces in the direction of the mean velocity gradient prevents that decay. In that case the buoyancy forces replenish the energy being drained out of the component of the turbulence in the direction of the mean velocity gradient, and the turbulent energy increases without limit as time increases. Apparently the energy can increase without limit because the effective Reynolds and Rayleigh numbers are infinite in an unbounded fluid. As the scale or mixing length of the turbulence continues to grow, the eddies encounter larger and larger velocity and temperature differences, so that the effective driving forces on the turbulence continue to grow.

Lewis Research Center,
National Aeronautics and Space Administration,
Cleveland, Ohio, July 6, 1970,
129-01.

# APPENDIX - SYMBOLS

a	vertical velocity gradient, ${ m dU}_1/{ m dx}_3$	$\gamma_{\mathbf{i}}$	defined by eq. (8)	
		Δ	defined by eq. (12)	
b	vertical temperature gradient,	δ	defined by eq. (9)	
	dT/dx <sub>3</sub>	$^{\delta}{}_{ij}$	Kronecker delta	
g	vertical body force/unit mass in -x <sub>3</sub> -direction (gravitational force/unit mass), -g <sub>3</sub>	$\theta, \varphi$	angular coordinates	
		$\kappa_{\mathbf{i}}$	wave number component	
$^{ m g}{}_{ m i}$	body force component/unit mass	$\kappa_0$	characteristic initial wave	
$^{\mathrm{g}}_{3}$	vertical body force/unit mass		number (see eq. (10))	
$^{ m J}{}_{ m O}$	constant that depends on initial	$\nu$	kinematic viscosity	
O	conditions	ρ	density	
$\Pr$	Prandtl number, $ u/lpha$	au	temperature fluctuation	
p	pressure	$\overline{ au_{f i}}$	temperature-velocity correlation	
Ri Richardso	βg dT/dx <sub>3</sub>	$arphi_{f ij}$	defined by eq. (7)	
	Richardson number, $\frac{\beta g \ dT/dx_3}{\left(dU_1/dx_3\right)^2}$	$\psi_{ m ij}$	defined by eq. (12)	
r, r <sub>i</sub>	vector between points P and P'	Subscripts:		
		1	in flow direction	
T	mean temperature	3	in vertical direction, which is	
t	time		direction of mean velocity gradient and buoyancy force	
t <sub>0</sub>	initial time			
U <sub>i</sub>	mean velocity component	Superso	ripts:	
-	fluctuating velocity component	7	at point P'	
u <sub>i</sub>	-		average	
x <sub>i</sub>	space coordinate	(a)	parameter nondimensionalized by quantities related to shear	
α	thermal diffusivity			
β	expansion coefficient	(b)	parameter nondimensionalized by	
$\Gamma_{f j}$	defined by eq. (12)		quantities related to buoyancy	

# REFERENCES

- 1. Deissler, Robert G.: Effects of Inhomogeneity and of Shear Flow in Weak Turbulent Fields. Phys. Fluids, vol. 4, no. 10, Oct. 1961, pp. 1187-1198.
- 2. Fox, J.: Velocity Correlations in Weak Turbulent Shear Flow. Phys. Fluids, vol. 7, no. 4, Apr. 1964, pp. 562-564.
- 3. Deissler, R. G.: Effect of Initial Condition on Weak Homogeneous Turbulence with Uniform Shear. Phys. Fluids, vol. 13, no. 7, July 1970, pp. 1868-1869.
- 4. Deissler, Robert G.: Effects of Combined Buoyancy and Shear on Weak Homogeneous Turbulence. NASA TN D-3999, 1967.
- 5. Deissler, Robert G.: Turbulence in the Presence of a Vertical Body Force and Temperature Gradient. J. Geophys. Res., vol. 67, no. 8, July 1962, pp. 3049-3062.
- 6. Loeffler, A.: Electric Field Modification of Turbulence in a Fluid Containing Space Charge. Grumman Research Dept. Rep. RE-384, July 1970. Grumman Aircraft Engineering Corp., Bethpage, N. Y.

OFFICIAL BUSINESS

#### FIRST CLASS MAIL



2 07U 001 37 51 3DS 70272 00903 AIR FORCE WEAPONS LABORATORY /WLOL/ KIRTLAND AFB, NEW MEXICO 87117

ATT E. LOU BOWMAN, CHIEF, TECH. LIBRARY

POSTMASTER: If Undeliverable (Section 158 Postal Manual) Do Not Return

"The aeronautical and space activities of the United States shall be conducted so as to contribute... to the expansion of human knowledge of phenomena in the atmosphere and space. The Administration shall provide for the widest practicable and appropriate dissemination of information concerning its activities and the results thereof."

-- NATIONAL AERONAUTICS AND SPACE ACT OF 1958

# NASA SCIENTIFIC AND TECHNICAL PUBLICATIONS

TECHNICAL REPORTS: Scientific and technical information considered important, complete, and a lasting contribution to existing knowledge.

TECHNICAL NOTES: Information less broad in scope but nevertheless of importance as a contribution to existing knowledge.

### TECHNICAL MEMORANDUMS:

Information receiving limited distribution because of preliminary data, security classification, or other reasons.

CONTRACTOR REPORTS: Scientific and technical information generated under a NASA contract or grant and considered an important contribution to existing knowledge.

TECHNICAL TRANSLATIONS: Information published in a foreign language considered to merit NASA distribution in English.

SPECIAL PUBLICATIONS: Information derived from or of value to NASA activities. Publications include conference proceedings, monographs, data compilations, handbooks, sourcebooks, and special bibliographies.

#### TECHNOLOGY UTILIZATION

PUBLICATIONS: Information on technology used by NASA that may be of particular interest in commercial and other non-aerospace applications. Publications include Tech Briefs, Technology Utilization Reports and Notes, and Technology Surveys.

Details on the availability of these publications may be obtained from:

SCIENTIFIC AND TECHNICAL INFORMATION DIVISION

NATIONAL AERONAUTICS AND SPACE ADMINISTRATION

Washington, D.C. 20546